Optimization and Design of a Diffuse Optical Wireless Sensor Network

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Wireless sensor networks (WSNs) are currently being deployed in everyday objects to collect and transmit information related to humidity, temperature, heartbeat, motion, etc. Such networks are part of the massive machine-type communication scenario (mMTC) within the fifth/sixth generation of wireless networks. In this paper, we consider the optimization and design of an optical WSN composed of multiple battery-powered sensor nodes based on light-emitting diode transmitters. Extending our previous work, we take into account both line-of-sight and diffuse light propagation, and show that in indoor scenarios, diffuse radiation can improve link availability under shadowing/blocking and extend battery life. In order to optimize the optical wireless link parameters, we use a machine-learning approach based on a genetic algorithm to ascertain the performance limits of the system. The presented results indicate that the proposed system is a viable wireless option for WSNs within the context of mMTC. © 2026 Optical Society of America

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1. INTRODUCTION

The internet-of-things (IoT) [1] constitutes one of the main drivers for the information and communication technology (ICT) industry. The fifth generation (5G) wireless networks have identified massive machine-type communications (mMTC) as a key enabler, encompassing use cases where multiple low-power sensor nodes (SNs) sporadically transmit information at relatively low data rates. Typical examples include smart-grids [2], smart cities [3], infrastructure monitoring [4], asset tracking [5], healthcare [6] and others. Wireless sensor networks (WSNs) composed of spatially distributed SNs within 5G/6G networks come with ever-increasing demands for higher energy efficiency and longer life spans [7].

WSNs offer unique features of network scalability, distributed control, etc. A range of radio frequency (RF) wireless technologies have been developed for industrial applications [8] but encounter problems such as tight wireless bandwidth resources, increased crosstalk (especially in multi-hop scenarios [9]), easy signal interception, fading, and relatively low power efficiency. Optical wireless communications (OWC) covering the infrared [10] and visible [11] part of the spectrum are being considered as part of future 5G/6G enabling technologies in certain applications, where RF-based system is not the preferred option [12]. Typical applications include smart manufacturing [13], information proclaiming to the public [14], underwater IoT [15], intelligent transportation [16], agriculture [17] and smart healthcare [18]. OWC-based WSN may offer higher data throughputs, inherent security, lower energy usage [13], [14]. However, due to the limitations of line-of-sight (LOS), energy-efficient network models and routing protocols must be used provided. In [19], an industrial monitoring system based on an optical camera communication system with an artificial neural network-based group detection mechanism for industry applications was proposed and implemented. In [20] and [21] channel modeling and characterization of indoor visible light communication for medical body-area networks were investigated. In [22] a triple-hop underwater WSN based on the hybrid RF and OWC links with the relay between the SNs and the access point was investigated by means of Monte-Carlo simulation. In [23], energy harvesting and energy efficient modulation schemes for VLC in industrial applications were investigated.

In [24], we studied an indoor OWC-based WSN using a VLC down-link and an infrared (IR) up-link to connect master nodes

(MN) and SNs. Considering LOS contribution only, one may obtain significant battery lifetimes. In this work, we adopt a more realistic system model accounting for the contribution of diffuse light resulting from beam reflections at various room surfaces. For relatively high data-rate links, such reflections will result in inter-symbol interference (ISI) [25]. However, for data rates considered in most IoT applications, which are generally low, we verify that the OWC channel can be considered approximately flat. Therefore, at the MN receiver, diffuse radiation simply adds up to the LOS component improving the signal-to-noise ratio (SNR). In order to optimize the WSN performance, we use a specially modified genetic algorithm (GA) [26], to obtain the optimal SN/MN arrangement considering the indoor environment (wall configuration, surface reflectivity, etc). We pay special attention to scenarios where no LOS power is received (e.g. due to blocking) and show that optimizing the transmitter beam-width can lead to significant power savings. The full implementation of our proposed approach is freely available under an open-source license [27].

The rest of the paper is organized as follows: in Section 2, we provide an overview of the WSN architecture and outline the basic design parameters of the physical layer. The system model encompassing both communication and energy consumption is outlined in Section 3. In Section 4, we highlight some details of the GA used for the design optimization. Section 5 presents the results obtained and their impact on WSN-based applications.

2. SYSTEM DESCRIPTION

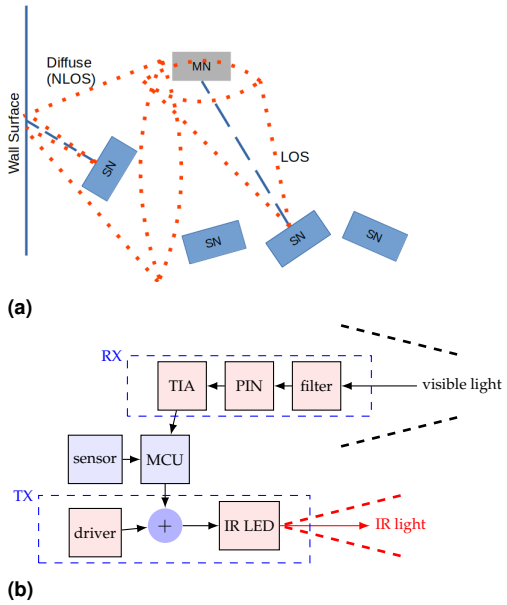


Fig. 1. (a) Hybrid VLC/IR network architecture (b) SN subsystem.

A. Architecture

The system under consideration is shown in Figure 1. Figure 1a shows a number of SNs that are periodically sending sensor readouts to one or multiple MNs using IR OWC up-links. The MN uses a VLC down-link to send acknowledgments and coordinate transmissions. Light signals transmitted from the SN can reach the MN through the LOS path or via multiple reflections from various surfaces of the room (diffuse path). Figure 1b shows the tranceiver diagram. At the transmitter (TX), the sensor information modulates the intensity of the IR LED(s) via the driver circuit. At the receiver (RX), an optical bandpass filter is used for limiting the ambient light noise prior to optical-to-electrical conversion using a PIN photodiode and a trans-impedance amplifier (TIA). In addition to the actual sensors, the node contains a micro-controller unit (MCU), which coordinates the node data transmission cycle. The MN architecture is similar except for exchanging the transmitting/receiving to use a LED-based VLC system for simultaneous communication and illumination.

We consider two rooms of different dimensions as outlined in Table 1. Configuration A is a small room and is identical to the one considered in [28], whereas configuration B is a larger room indicative of office spaces, storage rooms, etc. The reflectivity values in Table 1 correspond to typical white paint on plasterboard or acoustic tiles for the sidewalls/ceiling and light gray tiles for the floor.

B. Channel characteristics

The OWC channel is a linear, time invariant (LTI) system described by its impulse response $h(t)$. The LOS contribution is described by a Dirac delta function $h_{\mathrm{MN}}\delta(t-t_{\mathrm{MN}})$ [28], where h_{MN} is the LOS channel gain, $t_{\mathrm{MN}} = R_{\mathrm{MN}}/c$ the propagation delay between the SN and the MN, R_{MN} their distance and c the speed of light. The total impulse response $h(t)$ equals the sum of the LOS and the diffuse light component $h_{\mathrm{D}}(t)$, i.e.:

$$h(t) = h_{\mathrm{MN}}\delta(t-t_{\mathrm{MN}}) + h_{\mathrm{D}}(t) \quad \textbf{(1)}$$

We use an in-house `Python` implementation of the modified Monte Carlo ray-tracing method [29] to obtain $h_{\mathrm{D}}(t)$ and then use the fast Fourier transform (FFT) to determine the diffuse channel frequency response $H_{\mathrm{D}}(f) = \mathscr{F}\{h_{\mathrm{D}}(t)\}$, where $\mathscr{F}\{\cdot\}$ denotes the Fourier transform. We assume purely diffusive ideal Lambertian reflectors.

Figure 2 shows $H_D(f)$ obtained for the up-link for configurations A and B of Table 1 and for MN positioned in the middle of the ceiling, $\mathbf{r}_{\mathrm{MN}} = [L/2, W/2, H]$ while the SN is positioned at two different locations along the floor diagonal: $\mathbf{r}_{\mathrm{SN}} = \mathbf{r}_1 = [L/2, W/2, 0]$ and $\mathbf{r}_{\mathrm{SN}} = \mathbf{r}_2 = [L/4, W/4, 0]$. The SN and MN are directed according to Table 1. Figure 2a, corresponding to configuration A, shows that for both SN positions, $H_{\mathrm{D}}(f)$ varies in the MHz-range and can therefore be considered effectively flat in the sub-MHz frequency range. The half width 1 dB bandwidth $B_{1\mathrm{dB}}$ values of $|H_{\mathrm{D}}(f)|^2$ are 8.2 and 7.3 MHz for $\mathbf{r}_{\mathrm{SN}} = \mathbf{r}_1$ and $\mathbf{r}_{\mathrm{SN}} = \mathbf{r}_2$ respectively. A similar behavior is obtained for configuration B, where $B_{1\mathrm{dB}}$ is now 7.2 and 5.3 MHz for $\mathbf{r}_{\mathrm{SN}} = \mathbf{r}_1$ and $\mathbf{r}_{\mathrm{SN}} = \mathbf{r}_2$, respectively. These results indicate that the diffuse channel can be considered flat for WSN applications and can therefore be described by a scalar channel gain h'_{MN}. The total channel gain will simply be equal to the sum of the LOS and diffuse channel gains:

$$h^{\mathrm{TOT}}_{\mathrm{MN}} = h_{\mathrm{MN}} + h'_{\mathrm{MN}} \quad \textbf{(2)}$$

where

$$h'_{\mathrm{MN}} = \int_{-\infty}^{+\infty} h_{\mathrm{D}}(t)\mathrm{d}t \quad \textbf{(3)}$$

3. SYSTEM MODEL

There are two basic aspects of the physical layer model that we present in this section: the channel model discussed in subsection A and the transceiver model discussed in subsection B which includes power consumption.

Table 1. Simulation parameters

Parameter	Config. A	Config. B
Length, L	5 m	10 m
Width, W	5 m	10 m
Height, H	3 m	4 m
Window height, H_w	1 m	2 m
Window width, W_w	1 m	2 m
Peak spectral irradiance, p_n	$2\,W/nm/m^2$	
Ambient light temperature, T_K	5800 K	
Wall reflectivity, ρ_w	0.8	
Ceiling reflectivity, ρ_c	0.8	
Floor reflectivity, ρ_f	0.3	
MN field-of-view, FOV_{MN}	$\pi/2$	
SN field-of-view, FOV_{SN}	$\pi/2$	
MN orientation, $\mathbf{n}_{MN}$	$\hat{\mathbf{z}}$	
SN orientation, $\mathbf{n}_{SN}$	$-\hat{\mathbf{z}}$	
MN transmission power, P_{MN}	6 W	
Maximum SN transmission power, P_{SN}	25 mW	
IR LED half intensity angle, $\Phi_{1/2}$	60°	
IR LED pattern order, m	1	
IR LED driver curve	TSFF5210 [24]	
Max SN driver current, I_{max}	100 mA	
Responsivity model	BPV10NF [24]	
VLC rejection filter model	VTB5051BH [24]	
IR rejection filter model	BPV10NF [24]	
Maximum data rate, R_{max}	10 kb/s	
Target error rate, BER_0	10^{-3}	
Spectral efficiency, η_{eff}	0.4 bit/s/Hz	
Up-link message length, L_u	200 bits	
Down-link message length, L_d	200 bits	
Feedback resistance, R_F	1 MΩ	
Modulation type	OOK	
RMS voltage noise density, V_{rms}	$15\,nV/\sqrt{Hz}$	
RMS current noise density, V_{rms}	$400\,fA/\sqrt{Hz}$	
Voltage noise corner frequency, f_{cv}	1 kHz	
Current noise corner frequency, f_{ci}	1 kHz	
Sleep mode current, I_{SL}	400 nA	
Wake-up current, I_{WU}	1.3 mA	
Read out current, I_{RO}	1.3 mA	
Wake-up time, t_{WU}	20 ms	
Read-out time, t_{RO}	40 ms	
Cycle period, t_{CY}	1 min	
Battery capacity, Q_{TOT}	220 mAh	

A. Channel model

Assuming a generalized Lambertian-type TX of order m, located at $\mathbf{r} = \mathbf{r}_S$, oriented along the unitary vector $\mathbf{n}_S$, and a receiver placed at $\mathbf{r} = \mathbf{r}_R$, which is oriented along $\mathbf{n}_R$ and effective area A_R and field-of-view equal to FOV, the channel gain is determined by:

$$h(\mathbf{r}_R, \mathbf{n}_R, \mathbf{r}_S, \mathbf{n}_S) = \frac{m+1}{2\pi R^2} \cos^m \phi \cos\theta A_R U\left(\frac{\theta}{FOV}\right) \quad (4)$$

where

$$\cos\theta = \frac{\mathbf{n}_R \cdot (\mathbf{r}_S - \mathbf{r}_R)}{R} \quad (5a)$$

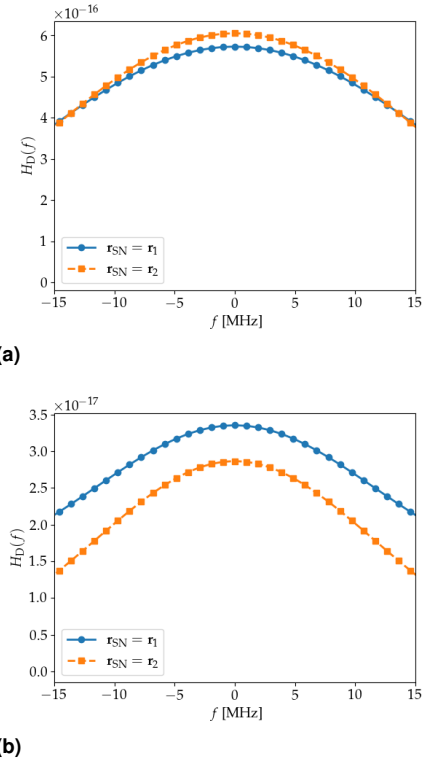


Fig. 2. Diffuse channel impulse response $|H_D(f)|$ for (a) configuration A and (b) configuration B.

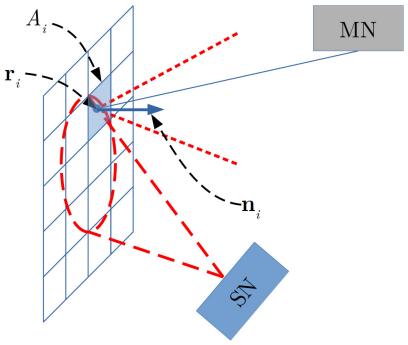


Fig. 3. Estimation of the diffuse light channel gain.

$$\cos\phi = \frac{\mathbf{n}_S \cdot (\mathbf{r}_R - \mathbf{r}_S)}{R} \quad (5b)$$

$$R = |\mathbf{r}_S - \mathbf{r}_R| \quad (5c)$$

As part of our optimizations and in order to avoid adopting time-consuming ray-tracing schemes as in Section B, we use a faster simulation method, where all room surfaces are represented by a collection of elementary sub-surfaces A_i, as shown in Figure 3. We first calculate the incident power $P_i^{(1)}$ on each A_i from the SN using Eq. (4), i.e., at the first light bounce. We also calculate the intra-subsurface LOS gain h_{qp} assuming A_p and A_q are the TX and RX, respectively. For A_p, the transmitted power is $r_p P_p^{(0)}$, where r_p is the reflectivity of A_p. Following the second bounce, the power received by A_q is written as the sum of powers received by all other elementary surfaces. More

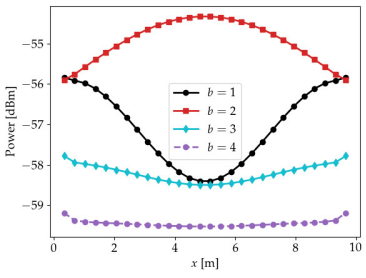
generally, the power received at the b^{th} bounce is given by:

$$P_q^{(b)} = \sum_{p=1}^{N_E} h_{qp} r_p P_p^{(b-1)} \tag{6}$$

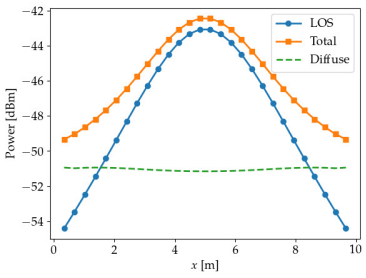
In Eq. (6), N_E is the number of elementary surfaces within the room. If h_q^{MN} are the channel gains assuming A_q is the TX and MN the RX, then the diffuse-light power $P_D^{(b)}$ is the sum of the received power from all A_q and therefore, the total diffuse power is given as:

$$P_D = \sum_{b=1}^{N_B} P_D^{(b)} = \sum_{b=1}^{N_B} \sum_{q=1}^{N_E} h_q^{MN} r_q P_q^{(b)} \tag{7}$$

where h_q^{MN} is the channel gain between A_q and the MN. Using Eq. (6) and Eq. (7) is analogous to the impulse response estimation adopted in [28], except that the channel here is considered to have flat response, and hence we simply add power contributions from consecutive bounces, speeding up computations significantly.



(a)



(b)

Fig. 4. a) Diffuse power contribution depending on bounce b and b) comparison of propagation path contribution to the received power.

Assuming the SN is positioned on various points along the diagonal $\mathbf{r}_{SN} = [x, x, 0]$ and its orientation is vertical, i.e. $\mathbf{n}_{SN} = \hat{\mathbf{z}}$, we have investigated the power distribution profiles $P_D^{(b)}$ in Figure 4a for configuration B. Interestingly enough, the power for $b = 1$ is smaller than $b = 2$. For $b = 1$, most of the IR power illuminates the ceiling elements and therefore lies outside the FOV of the MN. For $b = 2$, the MN captures optical power from sidewall elements that are now illuminated by the ceiling. Figure Eq. (4b), depicts the power distribution profiles for the LOS and diffuse paths, as well as the total power level for configuration B. Note that, near the center of the diagonal ($x \cong L/2$), the LOS path is much stronger than the diffuse path, whereas near its edges of the room, the diffuse component contributes greatly to the total received power.

B. Transceiver model and energy efficiency

The transceiver model includes the transmission spectra of nodes, RX filter spectra, photodiode responsivity, ambient light noise and TIA noise. Here we briefly describe the model features and the interested reader is referred to [24] for an in-depth analysis.

The SN transceiver is modeled based on the characteristics of the TSFF5210 IR LED and the VTB5051BH silicon photodiode with an IR rejection filter (Table 1). The IR LED transmission spectra $S_T(\lambda)$ is described by a Gaussian profile with a full width at half maximum (FWHM) of $\Delta\lambda = 40$ nm, peaking around $\lambda = 870$ nm. The optical power-current characteristic $P_T = f(I_D)$ is obtained by polynomial fitting of the actual light-current curve of TSFF5210. We assume a super-Gaussian profile for the IR rejection filter of order 3 with a 10dB bandwidth of 230 nm peaking at 435 nm while the responsivity $\mathcal{R}(\lambda)$ of the detector is described by a polynomial with respect to λ with coefficients extrapolated by curve-fitting from the BPV10NF responsivity.

The MN transceiver is modeled based on typical spectra of warm white phosphorescent LEDs. We describe the transmission spectra using a sum of two Gaussian profiles, corresponding to the blue and the phosphor components peaking at 470 and 600 nm, respectively, with FWHM equal to 20 and 100 nm, respectively. The daylight blocking filter is described by a 3rd order super-Gaussian peaking at 870 nm with a 10dB bandwidth of 300 nm. Given the spectral properties of the transceiver, we determine the effective responsivity $\mathcal{R}_{eff}$ describing the matching between the transmission spectra, the receiver's rejection filter and responsivity. Following the approach of [24], we obtain 0.49A/W and 0.32A/W for $\mathcal{R}_{eff}$ in the up-link and down-link, respectively.

The RX noise is mainly due to the ambient light-induced shot noise and the TIA thermal noise, where the former is usually dominant and can be characterized by its spectral irradiance, which in our model follows a black-body radiation model with an absolute temperature of 5800 K. Given the position and orientation of the emitting surfaces (e.g. windows), Eq. (4) can be modified to estimate the ambient light power incident at the RX. We assume a 1 and 4 m^2 window for configurations A and B, respectively, (Table 1) with peak spectral irradiance of 2 $W/nm/m^2$. We note that $\mathcal{R}_{eff}$ for ambient light is 0.09A/W for the MN and 0.13A/W for the SN [24]. Assuming on/off keying (OOK) modulation, then for a given SNR the transmit power P_T and thus the LED drive current I_D can be determined. The energy usage at the SN can be calculated considering the currents drawn by the transceiver and the MCU during various phases. Table 1 quotes typical values for each cycle [24]. Based on these, we can calculate the charge Q_{CY} drawn from the battery at each cycle and determine the node battery life-time t_{BL} given the battery capacity Q_{TOT} (assumed 220 mAh, typical of a coin-cell battery).

4. GENETIC ALGORITHM OPTIMIZATION

In Figure 5, we show the flowchart of the GA used to optimize the system parameters such as the SN orientation and data rate. Initially, we randomly choose a population consisting of N_{INIT} realizations of the system (chromosomes). The algorithm then proceeds to select candidates, by generating offsprings using a *crossover* operation, which transfers part of the parent genes to the offsprings. The genes of the offsprings are also *mutated*, i.e. randomly changed in an attempt to increase diversity. If a chromosome is produced that is stronger than the weakest

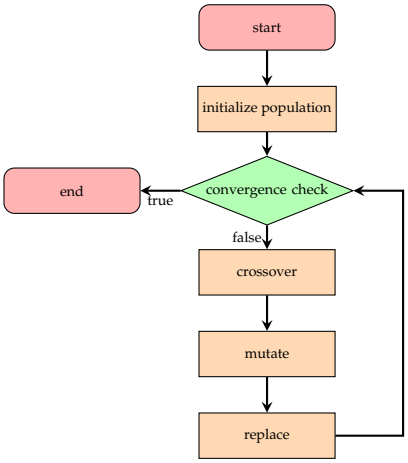


Fig. 5. The flowchart of the genetic algorithm used in this work.

chromosome in the existing pool, then the former chromosome is replaced by the latter. We then carry out a convergence check to see whether the algorithm's termination criteria are met and if not, we repeat the previous steps.

In each iteration, the strongest 50 % of the chromosomes constitute the mating pool. We choose two parents through tournament selection and we calculate the offspring using uniform crossover, which consists of tossing an unbiased coin and randomly selecting the value of each offspring gene from either the first or the second parent. The mutation is achieved by adding a random correction factor Δv_k to each of the offspring genes v_k. The corrections are determined by $\Delta v_k = \alpha \beta_k v_k$, where $0 \leq \alpha \leq 1$ is the *mutation factor*, and β_k are randomly chosen from a uniform distribution inside $[-1, 1]$. The chromosome values considered for the optimization are the inclination and azimuth angles θ and ϕ, respectively, as well as the data rate R_b. The angles determine the orientation of the SN, $\mathbf{n}_\mathrm{SN} = [\cos\phi \sin\theta, \sin\phi \sin\theta, \cos\theta]$, while R_b is related to the required bandwidth B and the transmission time t_TX. Note that, the strength of each chromosome is determined by a fitness function. In our case, we let the battery life t_BL determine the fitness of each system in order to optimize the energy efficiency at the SN. It is important to ensure that the maximum driving current should not exceed a specified value I_max due to the LED specifications, see Table 1. If this condition is not met, we set the fitness value equal to zero to avoid a non-viable solution.

The overall model including the GA which is available under an open-source license [27], is implemented in `Python` using standard libraries such as `numpy`, `scipy` and `matplotlib`. In order to speed-up the code execution, we choose to rely on vectorization, avoiding loops as much as possible. For example, it is much more efficient to determine all intra-channel gains h_{qp} simultaneously using a vector/matrix approach. In addition we only need to calculate h_{qp} once, since they only depend on the positioning and orientation of the sub-surfaces A_q. This speeds up the fitness evaluations considerably. In our simulations we also took advantage of `Python`'s `multiprocessing` package to distribute computations in multiple processes.

5. RESULTS AND DISCUSSIONS

In the proposed optimization scheme, we seek to determine the optimal values of $[\phi, \theta, R_\mathrm{b}]$ for every position in the floor diagonal $\mathbf{r}_\mathrm{SN} = [x, x, 0]$. We examine three cases: in the first and second variations, we only account for either the LOS or diffuse light power, respectively, when calculating t_BL. In the third variation, we sum up both contributions. The population has $N_\mathrm{INIT} = 50$ chromosomes and we use a mutation factor $\alpha = 0.1$. The algorithm terminates when either a maximum number of crossovers occurs (in our case 20000) or the population's fitness values f_i do not differ significantly from each other. We measure the population fitness smoothness $S = (f_\mathrm{max} - f_\mathrm{min})/f_\mathrm{max}$ where f_max and f_min are the maximum and minimum values of population fitnesses respectively. We terminate the algorithm if $S < 0.05\%$.

Figure 6a depicts the fitness function (i.e. t_BL) across the diagonal of the room $[x, x, 0]$ obtained by the GA for configuration A assuming LOS, diffuse and combination of both. It is interesting to note that the LOS component t_BL is symmetrical around 2.5 m with a peak value of 1400 days dropping at a rate of 400 day/m compared to the diffuse, which is almost flat at 750 day for the $0 \leq x \leq 5$ m. This is due to the fact that as the MN/SN distance is increased, the power budget worsens. Considering both LOS and diffuse components, energy efficiency is improved particularly near the edges of the diagonal. Figures 6b and 6c show the optimal elevation angle θ and the data rate R_b. For LOS, the optimal θ increases when we move away from the center ($x = 2.5$ cm) to better align with the MN, whereas the diffuse scenario favors $\theta \approx 0$, in which case the SN is almost pointing directly upwards, $\mathbf{n}_\mathrm{SN} \approx \hat{\mathbf{z}}$. The obtained data rate is given by $R_\mathrm{b} \approx 10$ kb/s $= R_\mathrm{max}$, which is the maximum allowable value given by system constraints. The fact that high R_b are favored can be explained through the RX electrical SNR in the case of OOK, given as:

$$\mathrm{SNR} = \frac{R_\mathrm{eff}^2 P_\mathrm{R}^2}{2\sigma^2} \tag{8}$$

where P_R is the received optical signal power (proportional to the transmit power P_T) and σ^2 is the RX noise power. Neglecting the TIA noise, we have $\sigma^2 = 2qI_\mathrm{amb}B$, where I_amb is the DC current due to ambient light, q is the electron charge, $B = R_\mathrm{b}/\eta_\mathrm{eff}$ the signal bandwidth and η_eff the spectral efficiency. Thus, with reference to Eq. (8), $P_\mathrm{T} \propto \sqrt{R_\mathrm{b}}$. Assuming linear light-current characteristic at the SN LED, we can also deduce that $I_\mathrm{D} \propto \sqrt{R_\mathrm{b}}$. Since the duration of the transmission phase t_TX is proportional to the bit duration $1/R_\mathrm{b}$, we readily see that the charge drawn from the node battery is $Q_\mathrm{TX} \propto 1/\sqrt{R_b}$. This implies that provided that $I_\mathrm{D} \leq I_\mathrm{max}$, increasing R_b leads to better energy efficiency.

Figure 7, shows the optimized results for configuration B. As shown in Figure 7a, the diffuse path offers the lowest battery lifetime with an average of ≈ 96 days. However it can still increase the overall battery lifetime considerably, especially at the edges of the diagonal. The optimal elevation angles exhibit a similar variation as those in Figure 6b, implying that if the diffuse component alone is considered the optimal SN orientation is still $\mathbf{n}_\mathrm{SN} \approx \hat{\mathbf{z}}$. As expected, the optimal SN elevation angles increase with the distance from floor center, in order to improve SN/MN alignment. Figure 7c depicts the optimal data rate, which is not always ≈ 10 kb/s since the required driving current must not exceed I_max. Considering only the diffuse component, the optimal $R_\mathrm{b} \approx 2$ kb/s. For the LOS component, R_b is much higher except for the points near the edge of the diagonal. Assuming both contributions from LOS and diffuse paths, we obtain an optimal data rate $\geq$5 kb/s for all SN positions considered (orange curve in Figure 7c).

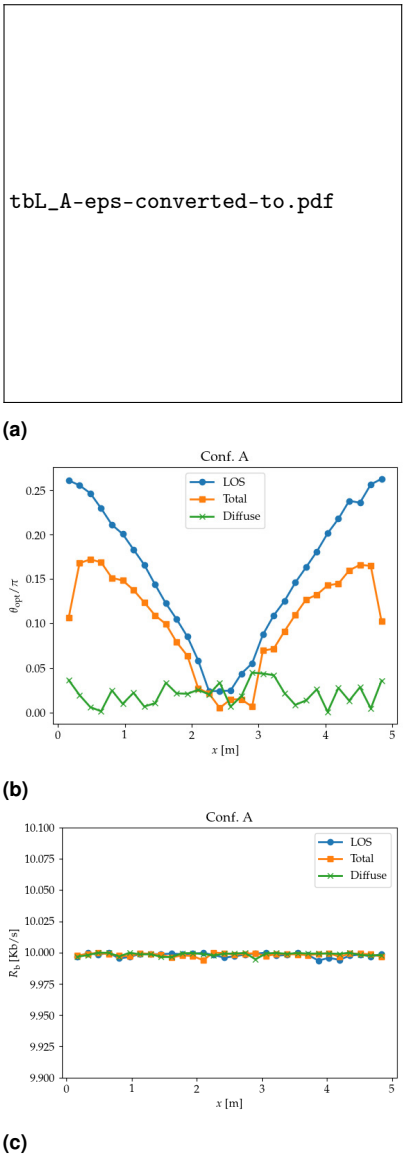


Fig. 6. Optimization results for room configuration A: a) battery lifetime, b) optimal elevation angle and c) optimal data rate

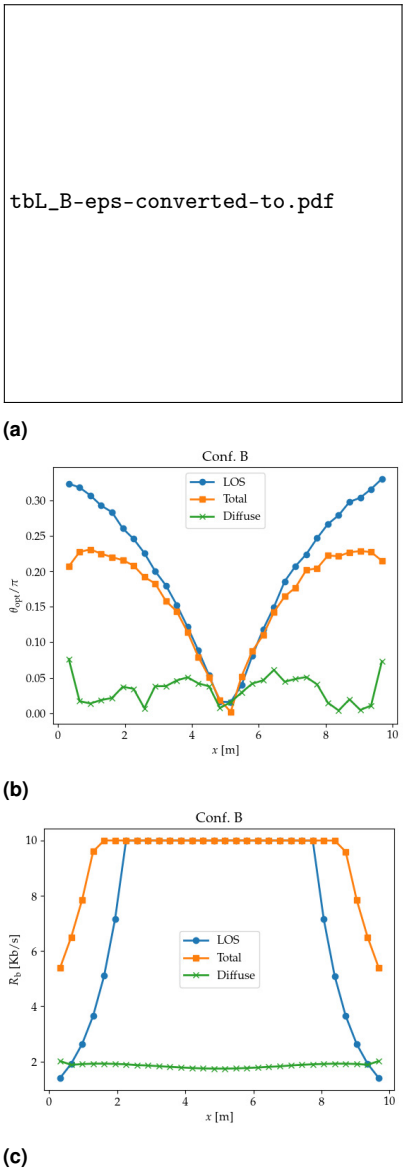


Fig. 7. Optimization results for room configuration B: a) battery lifetime, b) optimal elevation angle and c) optimal data rate

For the LOS path, an obvious way to improve link budget is to choose a smaller beam-width $\Phi_{1/2}$ thereby reducing beam spreading at the expense of tighter alignment control and limited mobility. It is interesting to investigate the optimal beam pattern for the diffuse path as well considering many possible positions for the SN. Figures 8 and 9, show the results for the two room configurations assuming that the beam-width $\Phi_{1/2}$ is also included in the optimization inside a range of $[10°, 20°]$. Figures 8a, 8b and **??** depict the values of t_{BL}, $\Phi_{1/2}$ and R_b respectively obtained for configuration A, assuming a 10×10 grid on the floor of the room. A minimum value of t_{BL} obtained was 890 days at the room corners. The optimal value for $\Phi_{1/2}$ was near 10°. This does not change even if we widen the allowed range for $\Phi_{1/2}$ in the GA, indicating a non-directed scenario where a tight beam impinges on the nearby room sidewall and light reaches the MN by a diffuse path. For all SN positions considered, the optimal R_b obtained is $\cong$ 10 kb/s. The results for configuration B are shown in Figure 9. In this case the minimum value of t_{BL} is 186 days and is maximized near the sidewalls reaching up to 450 days. Again, the algorithm favors beam-widths near 10° while the optimal data rate ranges from 3.6 kb/s to 9.4 kb/s.

6. CONCLUSIONS AND FUTURE DIRECTIONS

In this work, we presented a realistic model of describing a hybrid VLC/IR WSN, which included diffuse-light propagation. We showed that for typical data rates considered in most indoor mMTC applications, the diffuse channel can be considered flat and showed the significant contribution of the diffuse link in improving the up-link SNR at the MN. We used a GA to optimize the MN/SN configurations and showed that significant SN battery lifetimes can be obtained even for coin-cell battery capacities. We also investigated scenarios where only the diffuse light contribution was considered in the optimization and with the SN TX beam-width was considered as an optimization param-

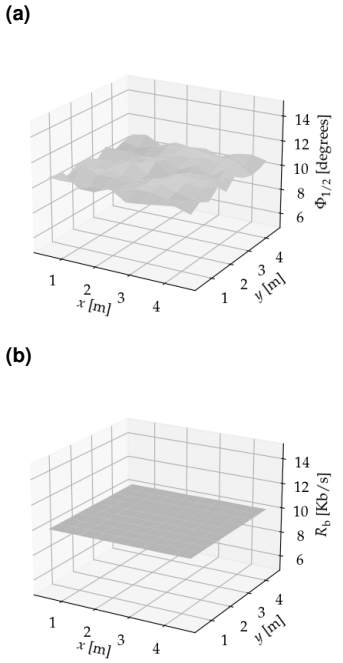


Fig. 8. Optimization results for diffuse light propagation configuration A: a) t_{BL}, b) $\Phi_{1/2}$ and c) R_b.

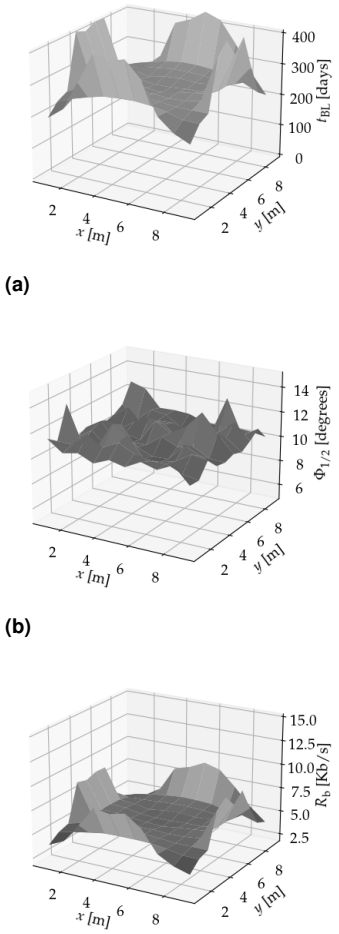


Fig. 9. Optimization results for diffuse light propagation configuration B: a) t_{BL}, b) $\Phi_{1/2}$ and c) R_b.

eter. The results presented in this work highlight the potential of OWC-based WSNs in future mMTC application within the context of 5G networks and beyond. For data rates envisioned in such applications, diffuse light propagation can improve the up-link power budget and improve energy efficiency. This is true for both small and larger room configurations such as the ones examined in this work. The optimizations show that when the LOS path is blocked, the diffuse channel actually favors non-directed configurations with narrower beam-widths where the IR light is aimed at the room's sidewall, reaching the MN via single and multiple bounces. Both our model and our optimization engine are available freely on the web under an open-source license for other researchers to use.

The results obtained in this paper point towards some interesting research directions to implement VLC/IR WSNs. A key question is whether the SN configuration can be changed in an adaptive manner. One could envision controlling the IR LED radiation pattern using micro-electromechanical systems [30] while the direction of transmission could be also be controlled by low-cost servo-motors mounted at the SN. It would also be interesting to develop algorithms for the real-time optimization of up-link performance that can converge quickly in order to limit power dissipation during the optimization stage. Another interesting scenario would be to investigate multi-hop scenarios where SNs, which are far from the MN or their LOS path can be blocked, communicate with the MN via other SNs to send reading to the MN. It is our intend to investigate some of these research questions in future research works.

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